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Computer Calculation of Fire Danger

ABSTRACT. — This paper describes a computer program that calculates National Fire Danger Rating Indexes. Fuel moisture, buildup index, and drying factor are also available. The program is written in FORTRAN and is usable on even the smallest compiler.

OXFORD: 431.5:U681.3

Since its introduction in 1964 the National Fire Danger Rating System has been adopted by most Federal and State forest fire control agencies, and has become an integral part of the decision-making process in fire control planning. Modern high-speed computers are an efficient tool for manipulating and analyzing the vast amount of fire danger data generated from this system. Using the National Fire Danger Rating System requires working with as many as five tables and seven variables. Danger ratings are obtained from this tabular method on a day-to-day basis. However, when mass conversion of historical weather data to the present system is required, the computer is an essential tool. In such cases a computer solution will speed up the calculations and provide computational accuracy.

This paper describes a computer program that computes buildup index, fire-load index, and various spread indexes. The program closely follows the method detailed by Nelson.¹ An equation computation method was chosen instead of a table look-up scheme for this program.² Primarily, the decision was dictated by computer memory limitations. Utilizing a look-up method would necessitate larger core size because of the 1,218 storage locations needed for the four tables.

The results from the formulas differ slightly from the table values. However, the differences are not great, and there is reason to believe that the computed results are more accurate than the tabular results.⁸

The flow chart (fig. 1) and listing of the program are included so the program may be used on the smallest FORTRAN compiler. The program has been thoroughly tested and run on an IBM 360/30 and requires less than 4K of memory. It uses the lowest possible level of FORTRAN, thus ensuring success on any machine.

For input, the program requires dry-bulb and wetbulb readings, a yes or no decision regarding snow on the ground, the preceding 24-hour precipitation, the current windspeed, yesterday's buildup index, and current herbaceous stage of vegetation. These are the same variables required by the tabular method.

¹ Nelson, Ralph M. The National Fire Danger Rating System: derivation of spread index for eastern and southern States. U.S.D.A. Forest Serv. Res. Pap. SE-13, 44 p., illus. (Southeast. Forest Exp. Sta., Asheville, N.C.). 1964.

² Barney, Richard J. Calculating the National Fire-Danger Rating Spread Index by computer. U.S.D.A. Forest Serv. Res. Note INT-19, 2 p. (Intermountain Forest, Range Exp. Sta., Ogden, Utah.) 1964.

³ Memorandum from John J. Keetch dated December 28, 1962. On file at North Central Forest Exp. Sta., St. Paul, Minn.

The program first tests for snow on the ground, a condition that results in spread index values of zero. If there is no snow, it calculates the fine fuel moisture and drying factor. Yesterday's buildup index is then adjusted for precipitation and the drying factor is added. Timber fuel moisture content is adjusted from the current buildup index. The fine fuel spread index and timber spread index are then calculated. The last step computes the fire-load rating, man-hour base.

The program calculates fine fuel spread, timber spread, buildup index recovery, and fire-load rating for each day. Additionally, fine fuel moisture, adjusted fuel moisture, and drying factor are also available, if desired.

The following formulas have been circulated in memoranda but have never been published. The formulas appear in the program and are reproduced here for greater emphasis and clarity.

Fine Fuel Moisture⁴

 $FFM = Ae^{B}$ (dry-wet)

Where

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Α	· B	Range of (dry-wet)
30.0	1,859	<ັ4.5° F. ́
19.2	0859	< 12.5° F.
13.8	0579	< 27.5° F.
22.5	· –.0774	> 27.5° F.

A and B are the piecewise regression coefficients used to determine FFM. The depression of the wet bulb is used to decide which set of A and B will be used. Herb stage is used to adjust the calculated fine fuel moisture by adding 5 percent for transition stage or 10 percent for green fuels.

Adjusted Fuel Moisture⁵

(50-Day Lag)

– BUI

ADFM = .9FFM + 9.5e 50.

Where — FFM is the current fine fuel moisture

BUI is today's buildup index recovery

e is the base of the natural logs

Adjusted fuel moisture is also equal to equivalent fuel moisture.

⁴ Memorandum from George M. Byram dated January 30, 1963. On file at North Central Forest Exp. Sta., St. Paul, Minn.

⁵ Memorandum from David Bruce dated March 1, 1963. On file at North Central Forest Exp. Sta., St. Paul, Minn.

Buildup Index³

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$$BUI = -50 \ (\log_{e} (1 - (-e \frac{BUO}{50.}))_{e} 1.175 \ (PRECIP - .1))$$

Where — BUI is today's buildup recovery corrected for any precipitation in the past 24 hours

BUO is yesterday's buildup

PRECIP is the past 24 hours precipitation in inches and hundredths

LOG e is the natural log is the base of natural logs

BUI must be adjusted by adding the drying factor *after* correction for any precipitation greater than 0.1 inch.

Fine Fuel Spread⁵

 $GRASS = A (WIND + B) (33. - FFM)^{1.65} -3.$

Timber Spread Index⁵

TIMBER = A (WIND + B) $(33. - ADFM)^{1.65} - 3.$

Where	Α	В	Windspeed
	0.01312	6.0	<14 m.p.h.
	0.009184	14.4	>14 m.p.h.

FFM = Fine fuel moisture

ADFM = Fuel moisture adjusted for 50-day timelag

WIND = Windspeed in m.p.h., 20 feet above open level ground

Fire Load Index⁶

(Man-Hour Base)

 $FLOAD = 10.^{(1.75(Log_{10} TIMBER) + .32 (Log_{10} BUI) - 1.64)}$

Where — TIMBER is the Timber Spread index

BUI is the buildup index recovery

Fire load index is not a feature of the National system, but has been suggested as an experimental feature for consideration.

⁶ Outline for discussion of fire load rating, prepared by John J. Keetch, undated. On file at North Central Forest Exp. Sta., St. Paul, Minn.

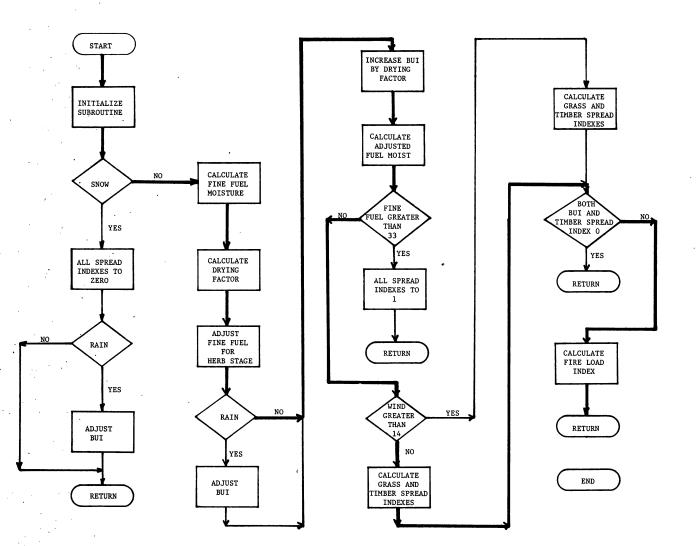


Figure 1. — Flow chart of subroutine to calculate National Fire Danger Rating Indexes.

 SUBROUTINE DANGER (DRY,WET,ISNOW, PRECIP,WIND,BUO,IHERB, DNGR 001
 DNGR 002

 ROUTINE FOR COMPUTING NATIONAL FIRE DANGER RATINGS AND FIRE LOAD INDEX
 DNGR 002

 ROUTINE FOR COMPUTING NATIONAL FIRE DANGER RATINGS AND FIRE LOAD INDEX
 DNGR 002

 DATA NEEDED FOR THE CALCULATIONS ARE=
 DNGR 002

 DWT, DRY BULB TEMPERATURE
 HET, WET BULB TEMPERATURE

 HET, WET BULB TEMPERATURE
 HET, WET BULB TEMPERATURE

 BUO, THE LAST VALUE OF THE BUILD UP INDEX
 DNGR 003

 BUO, THE LAST VALUE OF THE BUILD UP INDEX
 DATA RETURNED FROM THE SUBROUTINE ARE

 DATA RETURNED FROM THE SUBROUTINE ARE
 DF

 FINE FUEL MOISTURE AS
 DF

 FINE FUEL MOISTURE AS
 ADFM

 GRASS SPREAD INDEX MILL BE RETURNED AS
 FFM

 ADJUSTED (10 DAY LAG) FUEL MOISTURE AS
 ADFM

 GRASS SPREAD INDEX MILL BE RETURNED AS
 BUO

 DIFLOREX MILL BE RETURNED AS
 BUO

 DIFMESSION A(4),B(4),C(3),D(6)
 DNGR 003

 FFM 99.
 DNGR 007

 THESE ARE THE TABLE VALUES USED IN COMPUTING THE DANGER RATINGS
 A(1) = -0.185900

 A(1) = -0.185900
 DNGR 003
 DNGR 003

 A(1) = -0.285900
 DNGR 001
 DNGR 003

 A(1) = -0.285900

 TEST TO SEE IF THERE IS SHOW ON THE GROUND

 IF(ISNOW) 5,5,1
 DNGR 025

 THERE IS SNOW ON THE GROUND AND THE TIMBER AND GRASS SPREAD INDEXES
 MUST BE SET TO ZERO. WITH A ZERO TIMBER SPREAD THE FIRE LOAD IS

 ALSO ZERO. BUILD UP WILL BE ADJUSTED FOR PRECIPITATION.
 DNGR 026

 TIMBER-0.
 DNGR 027

 TF (PRECIP - 1.) 4,4,2
 DNGR 027

 SUD-50: #4LOG(1.-(1.-EXP (-BUO/50.))*EXP (-1.175*(PRECIP-1)))
 DNGR 027

 JE (BUO) 3,4,4
 DNGR 030

 SUD-50: #4LOG(1.-(1.-EXP (-BUO/50.))*EXP (-1.175*(PRECIP-1)))
 DNGR 030

 SUD-50: #4LOG(1.-(1.-EXP (-BUO/50.))*EXP (-1.175*(PRECIP-1)))
 DNGR 030

 SUD-50: #4LOG(1.-(1.-EXP (-BUO/50.))*EXP (-1.175*(PRECIP.-1)))
 DNGR 030

 SUD-50: #4LOG(1.-(1.-EXP (-BUO/50.))*EXP (-1.175*(PRECIP.-1)))
 DNGR 030

 SUD-50: #4LOG(1.-(1.-EXP (-BUO/50.))*EXP (-1.175*(PRECIP.-1)))
 DNGR 030

 AND FIRE LOAD
 DNGR 031

 DIF-50RY-WET
 DNGR 033

 DIF-50RY-WET
 DNGR 033

 O 6 I-1,3
 DNGR 033

 IF (DIF-c(1)) 7,7.6
 DNGR 033

 O KGR 031
 DNGR 033

 VO 8 I-1.6
 DNGR 033

 VO 8 I-1.6
 DNGR 033

DNGR 039 DNGR 040 DNGR 041 DNGR 042 DNGR 043 DNGR 044 9 DF=I-1

С

С

C C C

С

C C

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C TEST TO SEE IF THE FINE FUEL MOISTURE IS ONE OR LESS	
C IF FINE FUEL MOISTURE IS ONE OR LESS WE SET IT TO ONE	
10 IF (FFM-1.) 11,12,12 11 FFM=1.	DNGR 045
C ADD 5 PERCENT FINE FUEL MOISTURE FOR EACH HERB STAGE GREATER THA	DNGR 046
12 FFM = FFM + (IHERB-1) * 5.	DNGR 047
C WE MUST ADJUST THE BUI FOR PRECIPITATION BEFORE ADDING THE DRYIN	
IF (PRECIP1) 15,15,13	DNGR 048
a web of	
C PRECIPITATION EXCEEDED 0.10 INCHES WE MUST REDUCE THE	•
C BUILD UP INDEX (BUO) BY AN AMOUNT EQUAL TO THE RAIN FALL	
13 BU0=-50.*ALOG(1(1EXP (-BU0/50.))*EXP (-1.175*(PRECIP1)))	
IF (BUO) 14,15,15 14 BUO=0.0	DNGR 050 DNGR 051
C AFTER CORRECTION FOR RAIN, IF ANY, WE ARE READY TO ADD TODAY'S	
C DRYING FACTOR TO OBTAIN THE CURRENT BUILD UP INDEX	
15 BUO=BUO+DF	DNGR 052
C WE WILL ADJUST THE GRASS SPREAD INDEX FOR HEAVY FUEL LAGS C THE RESULT WILL BE THE TIMBER SPREAD INDEX	
C THE RESULT WILL BE THE TIMBER SPREAD INDEX C THE ADJUSTED FUEL MOISTURE, ADFM, ADJUSTED FOR HEAVY FUELS, WI	11
C NOW BE COMPUTED	
ADFM = .9*FFM +.5 +9.5*EXP (-BUO/50.)	DNGR 053
C TEST TO SEE IF THE FUEL MOISTURES ARE GREATER THAN 30 PERCENT.	
C IF THEY ARE, SET THEIR INDEX VALUES TO 1.	DNGR 054
IF (ADFM-30.) 19,16,16 16 IF (FFM-30.) 18,17,17	DNGR 055
C FINE FUEL MOISTURE IS GREATER THAN 30 PERCENT, THUS WE SET THE	GRASS
C AND TIMBER SPREAD INDEXES TO ONE.	
17 GRASS = 1. TIMBER = 1.	DNGR 056
RETURN	DNGR 057 DNGR 058
18 TIMBER = 1.	DNGR 059
C TEST TO SEE IF THE WIND SPEED IS GREATER THAN 14 MPH	
IF (WIND-14.) 21,25,25 19 IF (WIND-14.) 20,24,24	DNGR 060
19 1F (WIND-14.) 20,24,24 20 TIMPED = 01212#(WINDAS) # (22 _ADEW)##1 65 _ 2	DNGR 061 DNGR 062
20 TIMBER = .01312*(WIND+6.) * (33ADFM)**1.65 - 3. 21 GRASS = .01312*(WIND+6.*) * (33 FFM)**1.65 - 3.	DNGR 062
IF (TIMBER-1.) 22,22,28	DNGR 064
22 TIMBER = 1.	DNGR 065
IF (GRASS-1.) 23,28,28 23 GRASS = 1.	DNGR 066 DNGR 067
GO TO 28	DNGR 067
C WIND SPEED IS GREATER THAN 14 MPH. WE USE A DIFFERENT FORMULA	
24 TIMBER = .00918*(WIND+14.) * (33ADFM)**1.65 - 3.	DNGR 069
25 GRASS = .00918*(WIND+14.) * (33 FFM)**1.65 - 3.	DNGR 070
IF (GRASS-99.) 28,28,26	DNGR 071
26 GRASS = 99.	DNGR 072
IF (TIMBER-99.) 28,28,27	DNGR 073
27 TIMBER = 99.	DNGR 074
C WE HAVE NOW COMPUTED THE GRASS AND TIMBER SPREAD INDEXES C OF THE NATIONAL FIRE DANGER RATING SYSTEM. WE HAVE THE	
C BUILD UP INDEX AND NOW WE WILL COMPUTE THE FIRE LOAD RATING	
28 IF (TIMBER) 30,30,29	DNGR 075
29 IF (BUO) 30,30,31	DNGR 076
C IT IS NECESSARY THAT NEITHER TIMBER SPREAD NOR BUILD UP BE ZEI	
C IF EITHER TIMBER SPREAD OR BUILD UP IS ZERO, FIRE LOAD IS ZEF 30 RETURN	DNGR 077
C BOTH TIMBER SPREAD AND BUILD UP ARE GREATER THAN ZERO	
31 FLOAD=1.75*ALOG10(TIMBER) + .32*ALOG10(BUO) - 1.640	DNGR 078
C ENSURE THAT FLOAD IS GREATER THAN ZERO, OTHERWISE SET IT TO ZE	
IF (FLOAD) 32,32,33 32 FLOAD = 0.	DNGR 079 DNGR 080
RETURN	DNGR 081
33 FLOAD = 10. ** FLOAD	DNGR 082
RETURN	DNGR 083
END	DNGR 084

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